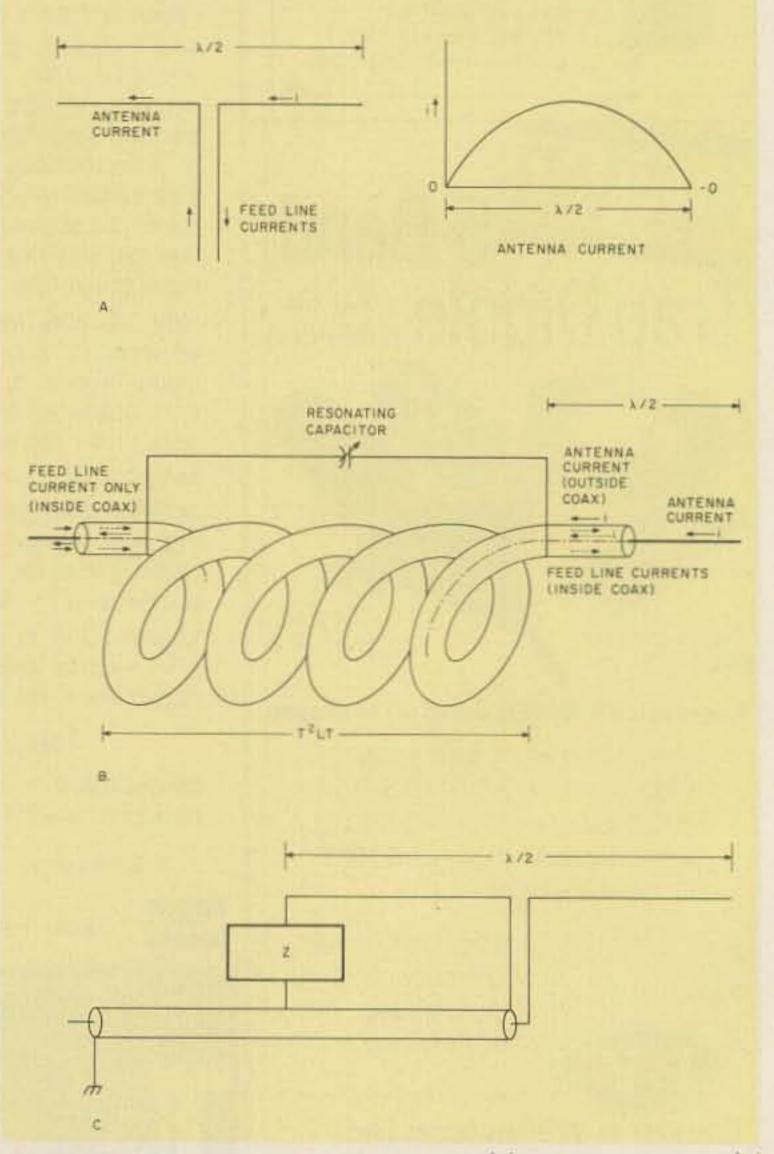
New Dipole Feeder – tuned feeders, yet!

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A previous article¹ of mine described the T²LT (Tuned Transmission Line Trap), its construction, and its use to prevent feedline radiation when used with a centerfed horizontal dipole. There are many applications antenna current of one side of a half-wave dipole, and it is



required for the unit to operate as a half-wave antenna. Fig. 2(a) shows the current distribution in a halfwave dipole, and Fig. 2(b) shows the corresponding current distribution in the T²LT endfed dipole. To behave as a half-wave dipole, the T²LT endfed antenna must have the same current distrubution on the outside of the coax shield as the dipole of Fig. 2(a). In particular, this current must go to zero at the ends of the dipole. The end of the wire insures zero current at the far end of the half-wave antenna, but the characteristic of the current at the T² LT end depends upon the impedance of the T²LT.

Impedance is defined as the ratio of the voltage to the current. Since the current at each end of a dipole antenna is zero, the impedance at the

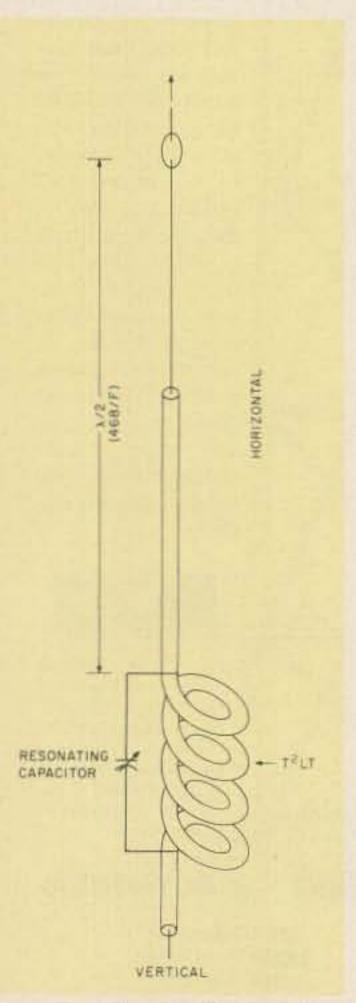
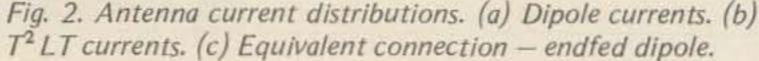


Fig. 1. The T^2LT endfed antenna.

for this unique device. The object of this article is to describe the use of the T^2LT to end feed either horizontal or vertical dipoles.

Fig. 1 shows a sketch of the T² LT used to end feed an antenna. The coil is made of the shield of the coaxial feedline; the capacitor is the value required to resonate the coil at the operating frequency. The number of turns in the coil may be as few as one. With a low number of turns, the resonating capacitor will be large, the Q high, and the bandwidth narrow. The antenna performance increases with the Q of the T² LT.

The T²LT operates in this application because of the ability of coaxial cable to simultaneously carry differing currents on the inside and the outside of the shield of the coax. Usually, a current flowing on the outside of the shield of a coaxial cable is undesirable. However, in this case, this outer current is the



ends of a dipole antenna cannot be defined. The only impedance that can be connected between the end of a dipole antenna and ground, without changing the current distribution of the antenna, is an infinite impedance. A parallel resonant tank circuit, theoretically, has infinite impedance across its terminals. Real, high-Q resonant tank circuits can have an impedance greater than 100,000 Ohms. A low-loss high-Q T² LT can, therefore, approach the desired infinite impedance.

Fig. 2(c) shows, topologically, how the impedance of the $T^2 LT$ is connected to one end of the half-wave dipole antenna. Fig. 3 shows the radiated power, measured at a distance of 10 wavelengths, from a 20 meter dipole as a function of the impedance connected between ground and one end of the antenna. Here it can be seen that a very high impedance is required of the $T^2 LT$ if the antenna is to perform properly.

Some authors^{2,3,4,5} have described an endfed dipole with an rf choke instead of a T²LT. These authors incorrectly presumed that the impedance at the end of a half-wave dipole antenna was defined and was approximately 4,000 Ohms. This, however, is the impedance of a half-wave radiator fed against an ideal ground plane,⁶ not the impedance at the end of a half-wave dipole. Fig. 3 indicates why these previously published designs of endfed dipoles have never become popular.

On the contrary, my T²LT vertical antennas have given excellent DX performance. Using a 2-Watt HW-7 on 20 meters, I consistently receive an S-8,9 report from VE6s in Calgary. That must be where the first skip lands.

Captain Lee⁷ discusses the advantages of a groundisolated vertical dipole but adds, "How one is to feed this antenna from a practical

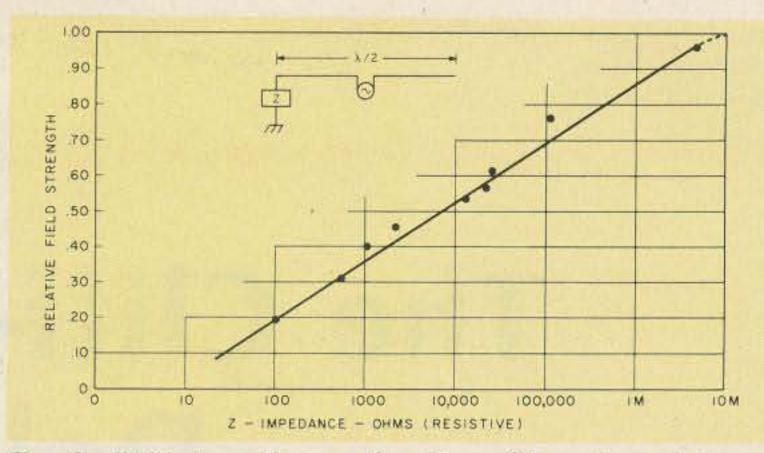


Fig. 3. Field strength as a function of impedance between dipole end and ground.

standpoint is never mentioned." I say, do it with a T²LT! The T²LT-fed vertical is ground independent and thereby avoids the extensive ground system required for conventional verticals.⁸ This antenna permits DX performance when using batterypowered, portable - even QRP - equipment. I have successfully used the $T^2 LT$ to feed shortened antennas, less than $\lambda/4$ in length, which answers the height problem associated with a half-wave vertical. The shortened antenna requires an appropriate

Radio Vertical Antenna Handbook, Cowan Publishing Corp., 1974, pp. 17.

⁸Sevick, J., ''The W2FMI Ground-Mounted Short Vertical,'' *QST*, March, 1973.

⁹ Sevick, J., "Broadbank Transmission Line Matching Networks," *Present and Future Trends in Communications Equipment Design*, 20-3, I.E.E.E., 1976.



Photo A. $T^2 LT$ of 10 meter vertical dipole.

unbalanced to unbalanced impedance matching transformer at the dipole center.⁹

Photos A and B show details of a T^2LT endfed antenna that was hastily constructed for OSCAR downlink communications. The T^2LT is simple to build, easy to adjust, and it outperforms conventional vertical antennas.

References

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²Orr, Wm. I. W6SA1, "Simple Low Cost Wire Antennas for Radio Amateurs," *Radio Publications, Inc.*, 1972, pp. 113-114. ³Orr, Wm. I. and Stuart D. Cowan, "The Truth About CB Antennas," *Radio Publications, Inc.*, pp. 154-155.

⁴ Kuecken, John A., Antennas and Transmission Lines, Howard W. Sams & Co., 1969, pp. 248-253. ⁵ Brueckman, H., "Theory and Performance of Vehicular Center-Fed Whip Antennas," IRE Trans. Vehicular Comm., Vol. VC-9, December, 1960, pp. 10-20. ⁶ King, R., The Theory of Linear Antennas, Harvard University Press, Cambridge MA, 1956. ⁷ Lee, Paul H., The Amateur

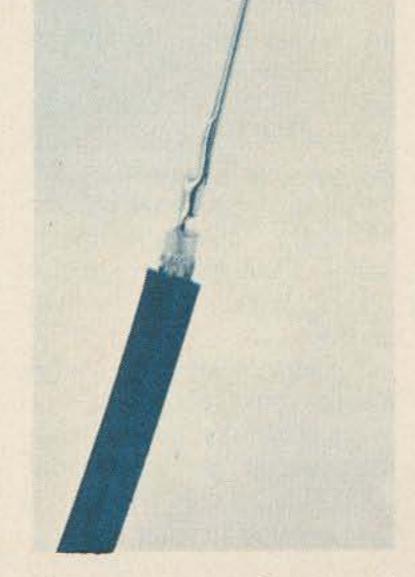


Photo B. Electrical center of T^2LT vertical antenna.